



نتایج مشروح محاسبات رله های E/F

 Company or Region Name = ZREC
 Group or Checker Name = Group_1
 Substation Name = Test_230kV_OK
 Voltage = 230 / 63 kV
 Calculation date & time = 2016 / 2 / 8 on Monday at 16:34:4
 Transformer(s) Type = Autotransformer
 S [Power Transformer(s) apparent power] = 160 MVA
 Sbase = 100 MVA
 Comment for this Calculation: محاسبات آزمایشی

..... Short circuit results :

Earth Fault Currents:

 جریان خطای تکفاز دیده شده توسط رله فیدرهای خروجی در حالت ماکزیمم سطح اتصال کوتاه شبکه و حضور ترانس های موازی

$$IE1(\text{Substation}) = 2.54 \text{ pu} \implies 2327.73 \text{ A}$$

جریان خطای تکفاز فیدرکوپلاژ در حالت ماکزیمم سطح اتصال کوتاه شبکه و حالت تک ترانسی بدون در نظر گرفتن اثر جریان تزریقی پست های مجاور متصل به فیدرهای خروجی

$$IE2(\text{Substation}) = 1.296 \text{ pu} \implies 1187.69 \text{ A}$$

جریان خطای تکفاز فیدر سمت اولیه در حالت ماکزیمم سطح اتصال کوتاه شبکه بدون در نظر گرفتن اثر جریان تزریقی پست های مجاور متصل به فیدرهای خروجی

$$IE3(\text{Substation}) = 32.42 \text{ pu} \implies 8138.13 \text{ A}$$

جریان خطای تکفاز فیدرهای خروجی در حالت مینیمم سطح اتصال کوتاه شبکه و حالت تک ترانسی

$$IE4(\text{Substation}) = 1.228 \text{ pu} \implies 1125.37 \text{ A}$$

حاصل تقسیم جریان خطای تکفاز فیدرکوپلاژ بر تعداد ترانس ها در حالت مینیمم سطح اتصال کوتاه شبکه و حضور ترانس های موازی

$$IE5(\text{Substation}) = 1.14 \text{ pu} \implies 1044.73 \text{ A}$$

جریان خطای تکفاز فیدر سمت اولیه در حالت مینیمم سطح اتصال کوتاه شبکه

$$IE6(\text{Substation}) = 10.899 \text{ pu} \implies 2735.89 \text{ A}$$

جریان های اتصال کوتاه زمین مورد استفاده در محاسبات

 leMax(1) = 2327.73 A
 leMax(2) = 1187.69 A
 leMax(3) = 1187.69 A
 leMax(4) = 1187.69 A
 leMax(5) = 8138.13 A
 leMax(6) = 1187.69 A



$I_{eMin}(1) = 1125.37 \text{ A}$
 $I_{eMin}(2) = 1044.73 \text{ A}$
 $I_{eMin}(3) = 1044.73 \text{ A}$
 $I_{eMin}(4) = 1044.73 \text{ A}$
 $I_{eMin}(5) = 2735.89 \text{ A}$
 $I_{eMin}(6) = 1044.73 \text{ A}$

-----<< E/F Protection >>-----
 Earth Fault Protective Relay R1(1) for 63 kV Outgoing Feeder 'A1'

Relay Type: MCGG82

Selected Characteristic: SI

Generic Formula: $T = (TMS/1) \times \{K / [(I/I_s)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times \{0.14 / [(I/I_s)^{0.02} - 1]^1 + 0\}$

$\alpha = 0.02$; $\beta = 0$; $\gamma = 1$; $K = 0.14$; $M = 1$

$I_n = 1 \text{ A}$; Relay Nominal Current

C.T Ratio = $I_1CT / I_2CT = 800 / 1$

Feeder type: Line

Connected to Section Nr. 1

Direction: Line side

$I_{base} = 916.43 \text{ A}$; Base Current

$I_{e1}(A1) = 2.541 \text{ pu} = 2328.65 \text{ A}$; Maximum 1-ph short circuit at forward Line beginning, seen by this Relay

$I_{e2}(A1) = 2.147 \text{ pu} = 1967.57 \text{ A}$; Maximum 1-ph short circuit at forward Line end, seen by this Relay

$I_{e5}(A1) = 0.92 \text{ pu} = 843.11 \text{ A}$; Minimum 1-ph short circuit, seen by this Relay

$ISR(A1) = 0.1 \times \text{Min}[I_1CT, I(LTR)] = 0.1 \times \text{Min}[800, 549] = 54.9 \text{ A}$

$I_s = [ISR(A1) / 800] \times I_n = 0.069 \times I_n$; Best Norm $\implies 0.1 \times I_n$

$ISR(A1) = 0.1 \times 800 = 80 \text{ A}$

Checking: $I_{e5}(A1) / ISR(A1) = 10.54$

$TMS(\text{Final}) = \text{Max} [\text{User defined TMS or Calculated TMS}] = 1$; Best Norm $\implies 1$

$I_{inst} = 1 \times [I_{e1} / ISR(A1)] \times I_s = 29.11 \times I_s$; Best Norm $\implies 29 \times I_s$

$T_{inst} = 0 \text{ sec}$; Norm $\implies 0 \text{ sec}$

Checking: $[(I_{e1} - I_{e2}) / I_{e1}] \times 100 = 15.5 \%$; !!!!!!! It is < 20 %

-----<< E/F Protection >>-----
 Earth Fault Protective Relay R1(2) for 63 kV Outgoing Feeder 'A2'

Relay Type: MCGG82

Selected Characteristic: SI

Generic Formula: $T = (TMS/1) \times \{K / [(I/I_s)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times \{0.14 / [(I/I_s)^{0.02} - 1]^1 + 0\}$



alfa = 0.02 ; Beta = 0 ; Gama = 1 ; K = 0.14 ; M = 1

In = 1 A ; Relay Nominal Current

C.T Ratio = I1CT / I2CT = 800 / 1

Feeder type: Line

Connected to Section Nr. 1

Direction: Line side

Ibase = 916.43 A ; Base Current

Ie1(A2) = 2.541 pu = 2328.65 A ; Maximum 1-ph short circuit at forward Line beginning, seen by this Relay

Ie2(A2) = 0.735 pu = 673.58 A ; Maximum 1-ph short circuit at forward Line end, seen by this Relay

Ie5(A2) = 0.5 pu = 458.21 A ; Minimum 1-ph short circuit, seen by this Relay

ISR(A2) = 0.1 × Min[I1CT, I(LTR)] = 0.1 × Min[800, 489] = 48.9 A

Is = [ISR(A2) / 800] × In = 0.061 × In ; Best Norm ==> 0.1 × In

ISR(A2) = 0.1 × 800 = 80 A

Checking: Ie5(A2) / ISR(A2) = 5.73

TMS according to required Relay Operating time for Faults in the Forward Line Beginning (Zone 1):

TMS1 = 0.4 × 1 / {0.14 / [(Ie1(A2) / ISR(A2)) ^ 0.02 - 1] + 0} = 0.199

TMS according to required Relay Operating time for Faults in the Forward Line End (Zone 2):

TMS2 = 0.8 × 1 / {0.14 / [(Ie2(A2) / ISR(A2)) ^ 0.02 - 1] + 0} = 0.249

TMS(Final) = Max [User defined TMS or Calculated TMS] = 0.249 ; Best Norm ==> 0.25

Iinst = 1 × [Ie1 / ISR(A2)] × Is = 29.11 × Is ; Best Norm ==> 29 × Is

Tinst = 0 sec; Norm ==> 0 sec

Checking: [(Ie1 - Ie2) / Ie1] × 100 = 71.1 %

-----<< E/F Protection >>-----

Earth Fault Protective Relay R1(3) for 63 kV Outgoing Feeder 'A3'

Relay Type: MCGG82

Selected Characteristic: SI

Generic Formula: T = (TMS/1) × {K / [(I/Is)^alfa - 1]^Gama + Beta} = (TMS/1) × {0.14 / [(I/Is)^0.02 - 1]^1 + 0}

alfa = 0.02 ; Beta = 0 ; Gama = 1 ; K = 0.14 ; M = 1

In = 1 A ; Relay Nominal Current

C.T Ratio = I1CT / I2CT = 800 / 1

Feeder type: Reactor



Connected to Section Nr. 1

Direction: Busbar side

$I_{base} = 916.43 \text{ A}$; Base Current

$I_{e3}(A3) = 1 \text{ pu} = 916.43 \text{ A}$; Maximum 1-ph short circuit at reverse Line beginning (if any)

$I_{e4}(A3) = 1 \text{ pu} = 916.43 \text{ A}$; Maximum 1-ph short circuit at reverse Line end (if any)

$I_{e5}(A3) = 0.83 \text{ pu} = 760.64 \text{ A}$; Minimum 1-ph short circuit, seen by this Relay

$ISR(A3) = 0.1 \times \text{Min}[I_{1CT}, I(LTR)] = 0.1 \times \text{Min}[800, 549] = 54.9 \text{ A}$

$I_s = [ISR(A3) / 800] \times I_n = 0.069 \times I_n$; Best Norm $\implies 0.1 \times I_n$

$ISR(A3) = 0.1 \times 800 = 80 \text{ A}$

Checking: $I_{e5}(A2) / ISR(A3) = 5.73$

Coordination with Line E/F Relays:

$T(A1) = 1 / 1 \times \{0.14 / [(I_{e3}(A3) / ISR(A1))^{0.02} - 1] + 0\} = 2.007 \text{ sec}$

$T(A3) = T(A1) + 0.4 = 2.407 \text{ sec}$

$TMS(A3) = 2.407 \times 1 / \{0.14 / [(I_{e3}(A3) / ISR(A3))^{0.02} - 1] + 0\} = 1.199$

Coordination with Line E/F Relays:

$T(A2) = 0.25 / 1 \times \{0.14 / [(I_{e3}(A3) / ISR(A2))^{0.02} - 1] + 0\} = 0.502 \text{ sec}$

$T(A3) = T(A2) + 0.4 = 0.902 \text{ sec}$

$TMS(A3) = 0.902 \times 1 / \{0.14 / [(I_{e3}(A3) / ISR(A3))^{0.02} - 1] + 0\} = 0.449$

$TMS(\text{Final}) = \text{Max} [\text{User defined TMS or Calculated TMS}] = 1.199$; Best Norm $\implies 1$

$I_{inst} = 1 \times [I_{e3} / ISR(A3)] \times I_s = 11.46 \times I_s$; Best Norm $\implies 11 \times I_s$

$T_{inst} = 0 \text{ sec}$; Norm $\implies 0 \text{ sec}$

-----<< E/F Protection >>-----
Earth Fault Protective Relay R1(4) for 63 kV Outgoing Feeder 'A4'

Relay Type: MCGG62

Selected Characteristic: SI

Generic Formula: $T = (TMS/1) \times \{K / [(I/I_s)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times \{0.14 / [(I/I_s)^{0.02} - 1]^1 + 0\}$

$\alpha = 0.02$; $\beta = 0$; $\gamma = 1$; $K = 0.14$; $M = 1$

$I_n = 1 \text{ A}$; Relay Nominal Current

C.T Ratio = $I_{1CT} / I_{2CT} = 800 / 1$

Feeder type: Cap-Bank

Connected to Section Nr. 2

Direction: Non Directional

$I_{base} = 916.43 \text{ A}$; Base Current



$I_{e1}(A4) = 2.5 \text{ pu} = 2291.07 \text{ A}$; Maximum 1-ph short circuit at forward Line beginning, seen by this Relay

$I_{e2}(A4) = 1.7 \text{ pu} = 1557.93 \text{ A}$; Maximum 1-ph short circuit at forward Line end, seen by this Relay

$I_{e3}(A4) = 1 \text{ pu} = 916.43 \text{ A}$; Maximum 1-ph short circuit at reverse Line beginning (if any), seen by this Relay

$I_{e4}(A4) = 1 \text{ pu} = 916.43 \text{ A}$; Maximum 1-ph short circuit at reverse Line end (if any), seen by this Relay

$I_{e5}(A4) = 0.9 \text{ pu} = 824.79 \text{ A}$; Minimum 1-ph short circuit, seen by this Relay

$ISR(A4) = 0.1 \times \text{Min}[I1CT, I(LTR)] = 0.1 \times \text{Min}[800, 549] = 54.9 \text{ A}$

$I_s = [ISR(A4) / 800] \times I_n = 0.069 \times I_n$; Best Norm ==> $0.05 \times I_n$

$ISR(A4) = 0.05 \times 800 = 40 \text{ A}$

Checking: $I_{e5}(A2) / ISR(A4) = 11.46$

Coordination with Line E/F Relays:

$T(A1) = 1 / 1 \times \{0.14 / [(I_{e3}(A4) / ISR(A1))^{0.02} - 1] + 0\} = 2.801 \text{ sec}$

$T(A4) = T(A1) + 0.4 = 3.201 \text{ sec}$

$TMS(A4) = 3.201 \times 1 / \{0.14 / [(I_{e3}(A4) / ISR(A4))^{0.02} - 1] + 0\} = 1.478$

Coordination with Line E/F Relays:

$T(A2) = 0.25 / 1 \times \{0.14 / [(I_{e3}(A4) / ISR(A2))^{0.02} - 1] + 0\} = 0.7 \text{ sec}$

$T(A4) = T(A2) + 0.4 = 1.1 \text{ sec}$

$TMS(A4) = 1.1 \times 1 / \{0.14 / [(I_{e3}(A4) / ISR(A4))^{0.02} - 1] + 0\} = 0.508$

$TMS(\text{Final}) = \text{Max} [\text{User defined TMS or Calculated TMS}] = 1.478$; Best Norm ==> 1

$I_{inst} = \text{Infinity}$

$T_{inst} = 0 \text{ sec}$; Norm ==> 0 sec

-----<< E/F Protection >>-----
 Earth Fault Protective Relay R2(1) for 63 KV at Buscoupler feeder 'Bus_LV_1'

Relay Type: MCGG82

Selected Characteristic: SI

Generic Formula: $T = (TMS/1) \times \{K / [(I/I_s)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times \{0.14 / [(I/I_s)^{0.02} - 1]^1 + 0\}$

$\alpha = 0.02$; $\beta = 0$; $\gamma = 1$; $K = 0.14$; $M = 1$

$I_n = 1 \text{ A}$; Relay Nominal Current

C.T Ratio = $I1CT / I2CT = 2000 / 1$

Feeder type: Bus-Coupler

Connected to Section Nr. 1

$I_n(\text{Transformer } 63 \text{ kV side}) = 160000 / (63 \times 3^{0.5}) = 1466.29 \text{ A}$

$ISR(\text{Bus_LV_1}) = 0.1 \times I_n(\text{Transformer } 63 \text{ kV side}) = 146.63 \text{ A}$



$I_s = [ISR(\text{Bus_LV_1}) / 2000] \times I_n = 0.073 \times I_n$; Best Norm $\implies 0.1 \times I_n$
 $ISR(\text{Bus_LV_1}) = 0.1 \times 2000 = 200 \text{ A}$

$I_{eMax}(A3) = 1187.69 \text{ A}$
 $TR(A3) = TMS(A3) / 1 \times \{0.14 / [(I_{eMax}(A3) / ISR(A3))^{0.02} - 1] + 0\} = 2.525 \text{ sec}$;
 Operating time for the Slowest Relay from lower layers
 $TR(\text{Bus_LV_1}) = TR(A3) + 0.4 = 2.925 \text{ sec}$

$TMS = TR(\text{Bus_LV_1}) \times 1 / \{0.14 / [I_{eMax}(A3) / ISR(\text{Bus_LV_1})]^{0.02} - 1\} + 0\} =$
 0.758 ; High Norm $\implies 0.775$

$l_{inst} = \text{Infinity}$
 $T_{inst} = 0 \text{ sec}$; Norm $\implies 0 \text{ sec}$

-----<< E/F Protection >>-----
 Earth Fault Protective Relay R4(1) for 63 KV at L.V Side feeder 'Trans_1'

Relay Type: MCGG22
 Selected Characteristic: SI
 Generic Formula: $T = (TMS/1) \times \{K / [(I/I_s)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times$
 $\{0.14 / [(I/I_s)^{0.02} - 1]^1 + 0\}$
 $\alpha = 0.02$; $\beta = 0$; $\gamma = 1$; $K = 0.14$; $M = 1$

$I_n = 1 \text{ A}$; Relay Nominal Current

C.T Ratio = $I_1CT / I_2CT = 600 / 1$
 Feeder type: Trans.
 Connected to Section Nr. 1

$ISR(\text{Trans_1}) = 0.1 \times ISR(\text{Bus_LV_1}) = 20 \text{ A}$
 $I_s = [ISR(\text{Trans_1}) / 600] \times I_n = 0.033 \times I_n$; Best Norm $\implies 0.1 \times I_n$
 $ISR(\text{Trans_1}) = 0.1 \times 600 = 60 \text{ A}$

$I_{eMax}(\text{Bus_LV_1}) = 1187.69 \text{ A}$
 $TR(\text{Bus_LV_1}) = TMS(\text{Bus_LV_1}) / 1 \times \{0.14 / [(I_{eMax}(\text{Bus_LV_1}) / ISR(\text{Bus_LV_1}))^{0.02} - 1] + 0\} = 2.991 \text{ sec}$; Operating time for the Slowest Relay from lower layers
 $TR(\text{Trans_1}) = TR(\text{Bus_LV_1}) + 0.4 = 3.391 \text{ sec}$

$TMS = TR(\text{Trans_1}) \times 1 / \{0.14 / [I_{eMax}(\text{Bus_LV_1}) / ISR(\text{Trans_1})]^{0.02} - 1\} + 0\}$
 $= 1.49$; Best Norm $\implies 1$

$l_{inst} = \text{Infinity}$
 $T_{inst} = 0 \text{ sec}$; Norm $\implies 0 \text{ sec}$

-----<< E/F Protection >>-----
 Earth Fault Protective Relay R4(2) for 63 KV at L.V Side feeder 'Trans_2'

Relay Type: MCGG22
 Selected Characteristic: SI



Generic Formula: $T = (TMS/1) \times \{K / [(I/Is)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times \{0.14 / [(I/Is)^{0.02} - 1]^1 + 0\}$
 $\alpha = 0.02$; $\beta = 0$; $\gamma = 1$; $K = 0.14$; $M = 1$

$I_n = 1$ A ; Relay Nominal Current

C.T Ratio = $I_1CT / I_2CT = 600 / 1$

Feeder type: Trans.

Connected to Section Nr. 2

$ISR(Trans_2) = 0.1 \times ISR(Bus_LV_1) = 20$ A

$I_s = [ISR(Trans_2) / 600] \times I_n = 0.033 \times I_n$; Best Norm $\implies 0.1 \times I_n$

$ISR(Trans_2) = 0.1 \times 600 = 60$ A

$I_{eMax}(Bus_LV_1) = 1187.69$ A

$TR(Bus_LV_1) = TMS(Bus_LV_1) / 1 \times \{0.14 / [(I_{eMax}(Bus_LV_1) / ISR(Bus_LV_1))^{\alpha} - 1] + 0\} = 2.991$ sec ; Operating time for the Slowest Relay from lower layers

$TR(Trans_2) = TR(Bus_LV_1) + 0.4 = 3.391$ sec

$TMS = TR(Trans_2) \times 1 / \{0.14 / [I_{eMax}(Bus_LV_1) / ISR(Trans_2)]^{\alpha} - 1] + 0\} = 1.49$; Best Norm $\implies 1$

$I_{inst} = \text{Infinity}$

$T_{inst} = 0$ sec; Norm $\implies 0$ sec

-----<< E/F Protection >>-----

Earth Fault Protective Relay R5(1) for 230 KV at Trans. Primary Side feeder 'HV_1'

Relay Type: MCGG22

Selected Characteristic: SI

Generic Formula: $T = (TMS/1) \times \{K / [(I/Is)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times \{0.14 / [(I/Is)^{0.02} - 1]^1 + 0\}$

$\alpha = 0.02$; $\beta = 0$; $\gamma = 1$; $K = 0.14$; $M = 1$

$I_n = 1$ A ; Relay Nominal Current

C.T Ratio = $I_1CT / I_2CT = 600 / 1$

Feeder type: Trans.

Connected to Section Nr. 1

$I_n(\text{Transformer } 230 \text{ kV side}) = 160000 / (230 \times 3^{0.5}) = 401.63$ A

$ISR(HV_1) = 0.2 \times I_n(\text{Transformer } 230 \text{ kV side}) = 80.33$ A

$I_s = [ISR(HV_1) / 600] \times I_n = 0.134 \times I_n$; Best Norm $\implies 0.15 \times I_n$

$ISR(HV_1) = 0.15 \times 600 = 90$ A

$I_{eMax}(Trans_1) = 1187.69$ A

$I'_{eMax}(Trans_1) = I_{eMax}(Trans_1) \times 0 = 0$ A



$I_{eMin}(Trans_1) = 1044.73 \text{ A}$
 $I'_{eMin}(Trans_1) = I_{eMin}(Trans_1) \times 0 = 0 \text{ A}$

Checking: $I'_{eMin}(Trans_1) / ISR(HV_1) = 0$
 $TR(Trans_1) = TMS(Trans_1) / 1 \times \{0.14 / [(I_{eMax}(Trans_1) / ISR(Trans_1))^{0.02} - 1] + 0\} = 2.275 \text{ sec}$; Operating time for the Slowest Relay from lower layers
 $TR(HV_1) = TR(Trans_1) + 0.3 = 2.575 \text{ sec}$

$TMS = TR(HV_1) \times 1 / \{0.14 / [I'_{eMax}(Trans_1) / ISR(HV_1)]^{0.02} - 1\} + 0 = -$
 18.393 ; Best Norm ==> 0.05

$l_{inst} = \text{Infinity}$
 $T_{inst} = 0 \text{ sec}$; Norm ==> 0 sec

-----<< E/F Protection >>-----
 Earth Fault Protective Relay R5(2) for 230 KV at Trans. Primary Side feeder 'HV_2'

Relay Type: MCGG22
 Selected Characteristic: SI
 Generic Formula: $T = (TMS/1) \times \{K / [(I/Is)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times$
 $\{0.14 / [(I/Is)^{0.02} - 1]^1 + 0\}$
 $\alpha = 0.02$; $\beta = 0$; $\gamma = 1$; $K = 0.14$; $M = 1$

$I_n = 1 \text{ A}$; Relay Nominal Current

$C.T \text{ Ratio} = I_1CT / I_2CT = 600 / 1$
 Feeder type: Trans.
 Connected to Section Nr. 1

$I_n(\text{Transformer } 230 \text{ kV side}) = 160000 / (230 \times 3^{0.5}) = 401.63 \text{ A}$

$ISR(HV_2) = 0.2 \times I_n(\text{Transformer } 230 \text{ kV side}) = 80.33 \text{ A}$
 $I_s = [ISR(HV_2) / 600] \times I_n = 0.134 \times I_n$; Best Norm ==> $0.15 \times I_n$
 $ISR(HV_2) = 0.15 \times 600 = 90 \text{ A}$

$I_{eMax}(Trans_2) = 1187.69 \text{ A}$
 $I'_{eMax}(Trans_2) = I_{eMax}(Trans_2) \times 0 = 0 \text{ A}$

$I_{eMin}(Trans_2) = 1044.73 \text{ A}$
 $I'_{eMin}(Trans_2) = I_{eMin}(Trans_2) \times 0 = 0 \text{ A}$

Checking: $I'_{eMin}(Trans_2) / ISR(HV_2) = 0$
 $TR(Trans_2) = TMS(Trans_2) / 1 \times \{0.14 / [(I_{eMax}(Trans_2) / ISR(Trans_2))^{0.02} - 1] + 0\} = 2.275 \text{ sec}$; Operating time for the Slowest Relay from lower layers
 $TR(HV_2) = TR(Trans_2) + 0.3 = 2.575 \text{ sec}$

$TMS = TR(HV_2) \times 1 / \{0.14 / [I'_{eMax}(Trans_2) / ISR(HV_2)]^{0.02} - 1\} + 0 = -$
 18.393 ; Best Norm ==> 0.05

$l_{inst} = \text{Infinity}$



Tinst = 0 sec; Norm ==> 0 sec

-----<< E/F Protection >>-----

Earth Fault Protective Relay R7(1) for 230 kV side Line Bay 'Abhar'

Relay Type: MCGG62

Selected Characteristic: SI

Generic Formula: $T = (TMS/1) \times \{K / [(I/Is)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times \{0.14 / [(I/Is)^{0.02} - 1]^1 + 0\}$

$\alpha = 0.02$; $\beta = 0$; $\gamma = 1$; $K = 0.14$; $M = 1$

In = 1 A ; Relay Nominal Current

C.T Ratio = I1CT / I2CT = 1200 / 4

Feeder type: Line

Connected to Section Nr. 1

Direction: Line side

Ibase = 251.02 A ; Base Current

Ie1(Abhar) = 24.68 pu = 6195.22 A ; Maximum 1-ph short circuit at forward Line beginning, seen by this Relay

Ie2(Abhar) = 12 pu = 3012.26 A ; Maximum 1-ph short circuit at forward Line end, seen by this Relay

Ie5(Abhar) = 5 pu = 1255.11 A ; Minimum 1-ph short circuit, seen by this Relay

ISR(Abhar) = Max [Ie5(Abhar) / 4 , 0.3 × CT.Rating] = 360 A

Is = [ISR(Abhar) / 300] × In = 1.2 × In ; Best Norm ==> 1.2 × In

ISR(Abhar) = 1.2 × 300 = 360 A

Checking: Ie5(Abhar) / ISR(Abhar) = 3.49

TMS according to required Relay Operating time for Faults in the Forward Line

Beginning (Zone 1):

$TMS1 = 0.4 \times 1 / \{0.14 / [(Ie1(Abhar) / ISR(Abhar))^{0.02} - 1] + 0\} = 0.167$

TMS according to required Relay Operating time for Faults in the Forward Line End

(Zone 2):

$TMS2 = 0.8 \times 1 / \{0.14 / [(Ie2(Abhar) / ISR(Abhar))^{0.02} - 1] + 0\} = 0.248$

TMS(Final) = Max [User defined TMS or Calculated TMS] = 0.248 ; High Norm ==> 0.25

linst = 0.9 × [Ie1 / ISR(Abhar)] × Is = 15.49 × Is ; Best Norm ==> 15 × Is

Tinst = 0 sec; Norm ==> 0 sec

Checking: $[(Ie1 - Ie2) / Ie1] \times 100 = 51.4 \%$

-----<< E/F Protection >>-----

Earth Fault Protective Relay R7(2) for 230 kV side Line Bay 'Eshragh'

Relay Type: MCGG22



Selected Characteristic: SI

Generic Formula: $T = (TMS/1) \times \{K / [(I/Is)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times \{0.14 / [(I/Is)^{0.02} - 1]^1 + 0\}$
 $\alpha = 0.02$; $\beta = 0$; $\gamma = 1$; $K = 0.14$; $M = 1$

$I_n = 1$ A ; Relay Nominal Current

C.T Ratio = $I_1CT / I_2CT = 1200 / 1$

Feeder type: Reactor

Connected to Section Nr. 1

Direction: Busbar side

$I_{base} = 251.02$ A ; Base Current

$I_{e3}(Eshragh) = 24.68$ pu = 6195.22 A ; Maximum 1-ph short circuit at reverse Line beginning (if any)

$I_{e4}(Eshragh) = 12$ pu = 3012.26 A ; Maximum 1-ph short circuit at reverse Line end (if any)

$I_{e5}(Eshragh) = 3.8$ pu = 953.88 A ; Minimum 1-ph short circuit, seen by this Relay

$ISR(Eshragh) = \text{Max} [0.3 \times \text{CT.Rating} , 1.1 \times (\text{Max } I_s(\text{all of E/F Relays that are Line side or Non Directional}))] = 396$ A

$I_s = [ISR(Eshragh) / 1200] \times I_n = 0.33 \times I_n$; Best Norm $\implies 0.35 \times I_n$

$ISR(Eshragh) = 0.35 \times 1200 = 420$ A

Checking: $I_{e5}(\text{Boein Zahra}) / ISR(Eshragh) = 2.27$

Coordination with H.V side or Relays in Lower layers:

$TR(HV_2) = 0.05 / 1 \times \{0.14 / [(I_{e3}(Eshragh) / ISR(HV_2))^{0.02} - 1] + 0\} = 0.079$ sec

$TMS5 = (TR(HV_2) + 0.3) \times 1 / \{0.14 / [(I_{e3}(Eshragh) / ISR(Eshragh))^{0.02} - 1] + 0\} = 0.15$

TMS according to required Relay Operating time for Faults in the Reverse Line beginning (Zone 1):

$TMS3 = 0.4 \times 1 / \{0.14 / [(I_{e3}(Eshragh) / ISR(Eshragh))^{0.02} - 1] + 0\} = 0.158$

TMS according to required Relay Operating time for Faults in the Reverse Line End (Zone 2):

$TMS4 = 0.8 \times 1 / \{0.14 / [(I_{e4}(Eshragh) / ISR(Eshragh))^{0.02} - 1] + 0\} = 0.23$

Coordination with Line E/F Relays:

$T(\text{Abhar}) = 0.25 / 1 \times \{0.14 / [(I_{e3}(Eshragh) / ISR(\text{Abhar}))^{0.02} - 1] + 0\} = 0.598$ sec

$T(Eshragh) = T(\text{Abhar}) + 0.4 = 0.998$ sec

$TMS(Eshragh) = 0.998 \times 1 / \{0.14 / [(I_{e3}(Eshragh) / ISR(Eshragh))^{0.02} - 1] + 0\} = 0.394$

$TMS(\text{Final}) = \text{Max} [\text{User defined TMS or Calculated TMS}] = 0.394$; High Norm $\implies 0.4$



$I_{inst} = 0.9 \times [I_{e3} / ISR(Eshragh)] \times I_s = 13.28 \times I_s$; Best Norm $\implies 13 \times I_s$
 $T_{inst} = 0$ sec; Norm $\implies 0$ sec

-----<< E/F Protection >>-----
 Earth Fault Protective Relay R7(3) for 230 kV side Line Bay 'Boein Zahra'

Relay Type: MCGG22

Selected Characteristic: SI

Generic Formula: $T = (TMS/1) \times \{K / [(I/I_s)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times \{0.14 / [(I/I_s)^{0.02} - 1]^1 + 0\}$

$\alpha = 0.02$; $\beta = 0$; $\gamma = 1$; $K = 0.14$; $M = 1$

$I_n = 1$ A ; Relay Nominal Current

C.T Ratio = $I_{1CT} / I_{2CT} = 1200 / 1$

Feeder type: Reactor

Connected to Section Nr. 2

Direction: Non Directional

$I_{base} = 251.02$ A ; Base Current

$I_{e1}(\text{Boein Zahra}) = 13.23$ pu = 3321.02 A ; Maximum 1-ph short circuit at forward Line beginning, seen by this Relay

$I_{e2}(\text{Boein Zahra}) = 8.04$ pu = 2018.22 A ; Maximum 1-ph short circuit at forward Line end, seen by this Relay

$I_{e3}(\text{Boein Zahra}) = 24.68$ pu = 6195.22 A ; Maximum 1-ph short circuit at reverse Line beginning (if any), seen by this Relay

$I_{e4}(\text{Boein Zahra}) = 12$ pu = 3012.26 A ; Maximum 1-ph short circuit at reverse Line end (if any), seen by this Relay

$I_{e5}(\text{Boein Zahra}) = 3.8$ pu = 953.88 A ; Minimum 1-ph short circuit, seen by this Relay

$ISR(\text{Boein Zahra}) = \text{Max} [I_{e5}(\text{Boein Zahra}) / 4 , 0.3 \times \text{CT.Rating} , 1.1 \times (\text{Max } I_s(\text{all of E/F Relays that are Line side or Non Directional}))] = 396$ A

$I_s = [ISR(\text{Boein Zahra}) / 1200] \times I_n = 0.33 \times I_n$; Best Norm $\implies 0.35 \times I_n$

$ISR(\text{Boein Zahra}) = 0.35 \times 1200 = 420$ A

Checking: $I_{e5}(\text{Boein Zahra}) / ISR(\text{Boein Zahra}) = 2.27$

Coordination with H.V side or Relays in Lower layers:

$TR(HV_2) = 0.05 / 1 \times \{0.14 / [(I_{e3}(\text{Boein Zahra}) / ISR(HV_2))]^{0.02} - 1\} + 0\} = 0.079$ sec

$TMS5 = (TR(HV_2) + 0.3) \times 1 / \{0.14 / [(I_{e3}(\text{Boein Zahra}) / ISR(\text{Boein Zahra}))^{0.02} - 1] + 0\} = 0.15$

Coordination with Line E/F Relays:

$T(\text{Abhar}) = 0.25 / 1 \times \{0.14 / [(I_{e3}(\text{Boein Zahra}) / ISR(\text{Abhar}))^{0.02} - 1] + 0\} = 0.598$ sec

$T(\text{Boein Zahra}) = T(\text{Abhar}) + 0.4 = 0.998$ sec

$TMS(\text{Boein Zahra}) = 0.998 \times 1 / \{0.14 / [(I_{e3}(\text{Boein Zahra}) / ISR(\text{Boein Zahra}))^{0.02} - 1] + 0\}$



$$0.02 - 1] + 0\} = 0.394$$

TMS(Final) = Max [User defined TMS or Calculated TMS] = 0.449 ; High Norm ==> 0.45

linst = $1.3 \times [I_{e1} / \text{ISR}(\text{Boein Zahra})] \times I_s = 10.28 \times I_s$; Best Norm ==> $10 \times I_s$

Tinst = 0 sec; Norm ==> 0 sec

Checking: $[(I_{e1} - I_{e2}) / I_{e1}] \times 100 = 39.2 \%$

-----<< E/F Protection >>-----

Earth Fault Protective Relay, R8(1) for 230 kV side Buscoupler feeder 'Bus_HV'

Relay Type: MCGG82

Selected Characteristic: SI

Generic Formula: $T = (\text{TMS}/1) \times \{K / [(I/I_s)^{\alpha} - 1]^{\gamma} + \beta\} = (\text{TMS}/1) \times \{0.14 / [(I/I_s)^{0.02} - 1]^1 + 0\}$

$\alpha = 0.02$; $\beta = 0$; $\gamma = 1$; $K = 0.14$; $M = 1$

$I_n = 1$ A ; Relay Nominal Current

C.T Ratio = $I_{1CT} / I_{2CT} = 2000 / 1$

Feeder type: Bus-Coupler

Connected to Section Nr. 1

$I_{base} = 251.02$ A ; Base Current

$I_{e1Max}(\text{Bus_HV}) = 32.42 \text{ Pu} = 29710.63$ A ; Maximum 1-ph short circuit at Line beginning, seen by this Relay

$I_{e2Max}(\text{Bus_HV}) = 14 \text{ Pu} = 12830.01$ A ; Maximum 1-ph short circuit at smallest Line end, seen by this Relay

$I_{e3Min}(\text{Bus_HV}) = 7 \text{ Pu} = 6415$ A ; Minimum 1-ph short circuit, seen by this Relay

$\text{ISR}(\text{Bus_HV}) \geq 0.2 \times I_{1ct}(\text{H.V}) = 400$ A

$\text{ISR}(\text{Bus_HV}) \geq 360$ A ; According to Current setting of Abhar

$\text{ISR}(\text{Bus_HV}) \geq 420$ A ; According to Current setting of Boein Zahra

ISR = Maximum all of ISRs = 420 A

$I_s = [\text{ISR}(\text{Bus_HV}) / 2000] \times I_n = 0.21 \times I_n$; Best Norm ==> $0.2 \times I_n$

$\text{ISR}(\text{Bus_HV}) = 0.2 \times 2000 = 400$ A

Checking: $I_{e3min}(\text{Bus_HV}) / \text{ISR}(\text{Bus_HV}) = 16.04$

TMS(Final) = Max [User defined TMS or Calculated TMS] = 1 ; High Norm ==> 1

linst = Infinity

Tinst = 0 sec; Norm ==> 0 sec

-----<< E/F Protection >>-----

Earth Fault Protective Relay R9(1) for 230 kV side Neutral Protection at feeder 'HV_Neutral_1'

Relay Type: MCGG22



Selected Characteristic: SI

Generic Formula: $T = (TMS/1) \times \{K / [(I/Is)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times \{0.14 / [(I/Is)^{0.02} - 1]^1 + 0\}$

$\alpha = 0.02$; $\beta = 0$; $\gamma = 1$; $K = 0.14$; $M = 1$

$I_n = 1$ A ; Relay Nominal Current

C.T Ratio = $I_{1CT} / I_{2CT} = 1200 / 1$

Feeder type: Trans.

Connected to Section Nr. 1

$I_{base} = 251.02$ A ; Base Current

$I_{e1Max}(HV_Neutral_1) = 32.42$ Pu = 29710.63 A ; Maximum 1-ph short circuit at Line beginning, seen by this Relay

$I_{e2Max}(HV_Neutral_1) = 1$ Pu = 916.43 A ; Maximum 1-ph short circuit at smallest Line end, seen by this Relay

$I_{e3Min}(HV_Neutral_1) = 1$ pu = 916.43 A ; Minimum 1-ph short circuit, seen by this Relay

$I_L(H.V) = 160000 / (230 \times 3^{0.5}) = 401.63$ A ; Trans. Nominal Current at 230 kV side

$ISR(HV_Neutral_1) \geq 0.3 \times I_L(H.V) = 120.49$ A

$I_s = [ISR(HV_Neutral_1) / 1200] \times I_n = 0.1 \times I_n$; Best Norm $\implies 0.1 \times I_n$

$ISR(HV_Neutral_1) = 0.1 \times 1200 = 120$ A

$I_{eMax}(Trans_1) = 1187.69$ A

$I'_{eMax}(Trans_1) = I_{eMax}(Trans_1) \times 0 = 0$ A

$I_{eMin}(Trans_1) = 1044.73$ A

$I'_{eMin}(Trans_1) = I_{eMin}(Trans_1) \times 0 = 0$ A

Checking: $I'_{eMin}(Trans_1) / ISR(HV_Neutral_1) = 0$

$TR(Trans_1) = TMS(Trans_1) / 1 \times \{0.14 / [(I_{eMax}(Trans_1) / ISR(Trans_1))^{0.02} - 1] + 0\} = 2.275$ sec ; Operating time for the Slowest Relay from lower layers

$TR(HV_Neutral_1) = TR(Trans_1) + 0.4 = 2.675$ sec

$TMS = TR(HV_Neutral_1) \times 1 / \{0.14 / [I'_{eMax}(Trans_1) / ISR(HV_Neutral_1)]^{0.02} - 1] + 0\} = -19.107$; High Norm $\implies 0.05$

Checking: $I_{e3min}(HV_Neutral_1) / ISR(HV_Neutral_1) = 7.64$

Coordination with Remote substation's Relay or Fuse (You may deactivate this option):

Time of Extra Relay or Fuse = 2 sec ; Slowest Relay Operating time for I_{e6}

$TR6(HV_Neutral_1) = 1 + 2 = 3$ sec

$I_{e6}(HV_Neutral_1)$; Maximum common current with Extra Relay, seen by this Relay = 2 pu = 502.04 A

$TMS6 = 3 \times 1 / \{0.14 / [(I_{e6}(HV_Neutral_1) / ISR(HV_Neutral_1))^{0.02} - 1] + 0\} = 0.622$



TMS(Final) = Max [User defined TMS or Calculated TMS] = 0.622 ; High Norm ==> 0.625

linst = Infinity

Tinst = 0 sec; Norm ==> 0 sec

-----<< E/F Protection >>-----

Earth Fault Protective Relay R9(2) for 230 kV side Neutral Protection at feeder 'HV_Neutral_2'

Relay Type: MCGG22

Selected Characteristic: SI

Generic Formula: $T = (TMS/1) \times \{K / [(I/Is)^{\alpha} - 1]^{\gamma} + \beta\} = (TMS/1) \times \{0.14 / [(I/Is)^{0.02} - 1]^1 + 0\}$

alfa = 0.02 ; Beta = 0 ; Gama = 1 ; K = 0.14 ; M = 1

In = 1 A ; Relay Nominal Current

C.T Ratio = I1CT / I2CT = 1200 / 1

Feeder type: Trans.

Connected to Section Nr. 2

Ibase = 251.02 A ; Base Current

Ie1Max(HV_Neutral_2) = 32.42 Pu = 29710.63 A ; Maximum 1-ph short circuit at Line beginning, seen by this Relay

Ie2Max(HV_Neutral_2) = 1 Pu = 916.43 A ; Maximum 1-ph short circuit at smallest Line end, seen by this Relay

Ie3Min(HV_Neutral_2) = 1 pu = 916.43 A ; Minimum 1-ph short circuit, seen by this Relay

IL(H.V) = 160000 / (230 × 3^{0.5}) = 401.63 A ; Trans. Nominal Current at 230 kV side

ISR(HV_Neutral_2) ≥ 0.3 × IL(H.V) = 120.49 A

Is = [ISR(HV_Neutral_2) / 1200] × In = 0.1 × In ; Best Norm ==> 0.1 × In

ISR(HV_Neutral_2) = 0.1 × 1200 = 120 A

IeMax(Trans_2) = 1187.69 A

I'eMax(Trans_2) = IeMax(Trans_2) × 0 = 0 A

IeMin(Trans_2) = 1044.73 A

I'eMin(Trans_2) = IeMin(Trans_2) × 0 = 0 A

Checking: I'eMin(Trans_2) / ISR(HV_Neutral_2) = 0

TR(Trans_2) = TMS(Trans_2) / 1 × {0.14 / [(IeMax(Trans_2) / ISR(Trans_2))^{0.02} - 1] + 0} = 2.275 sec ; Operating time for the Slowest Relay from lower layers

TR(HV_Neutral_2) = TR(Trans_2) + 0.4 = 2.675 sec

TMS = TR(HV_Neutral_2) × 1 / {0.14 / [(I'eMax(Trans_2) / ISR(HV_Neutral_2))^{0.02} - 1] + 0} = -19.107 ; High Norm ==> 0.05



Checking: $I_{e3min}(HV_Neutral_2) / ISR(HV_Neutral_2) = 7.64$

TMS according to required Relay Operating time for Faults in the Forward Line Beginning (Zone 1):

$$TMS1 = 0.5 \times 1 / \{0.14 / [(I_{e1}(HV_Neutral_2) / ISR(HV_Neutral_2)) ^ 0.02 - 1] + 0\} = 0.416$$

TMS according to required Relay Operating time for Faults in the Forward Line End (Zone 2):

$$TMS2 = 1 \times 1 / \{0.14 / [(I_{e2}(HV_Neutral_2) / ISR(HV_Neutral_2)) ^ 0.02 - 1] + 0\} = 0.296$$

TMS(Final) = Max [User defined TMS or Calculated TMS] = 0.416 ; High Norm ==> 0.425

linst = Infinity

Tinst = 0 sec; Norm ==> 0 sec